

A photograph of an offshore wind farm with several white wind turbines in a blue sea under a clear blue sky. The Siemens logo is in the top right corner.

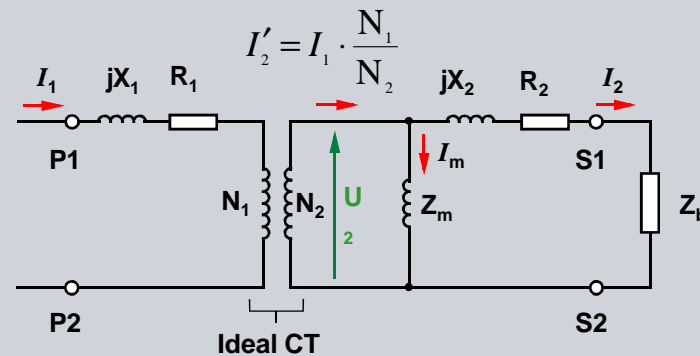
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# Current and Voltage Transformers Performance Requirements

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Energy Sector

# Equivalent current transformer circuit

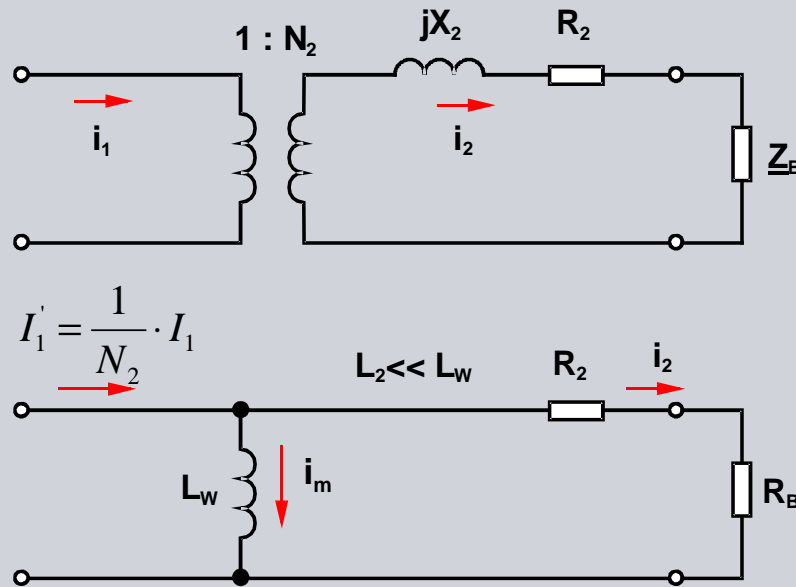
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$X_1$  = Primary leakage reactance  
 $R_1$  = Primary winding resistance  
 $X_2$  = Secondary leakage reactance  
 $Z_m$  = Magnetizing impedance  
 $R_2$  = Secondary winding resistance  
 $Z_b$  = Secondary load

Note: Normally the leakage fluxes  $X_1$  and  $X_2$  can be neglected

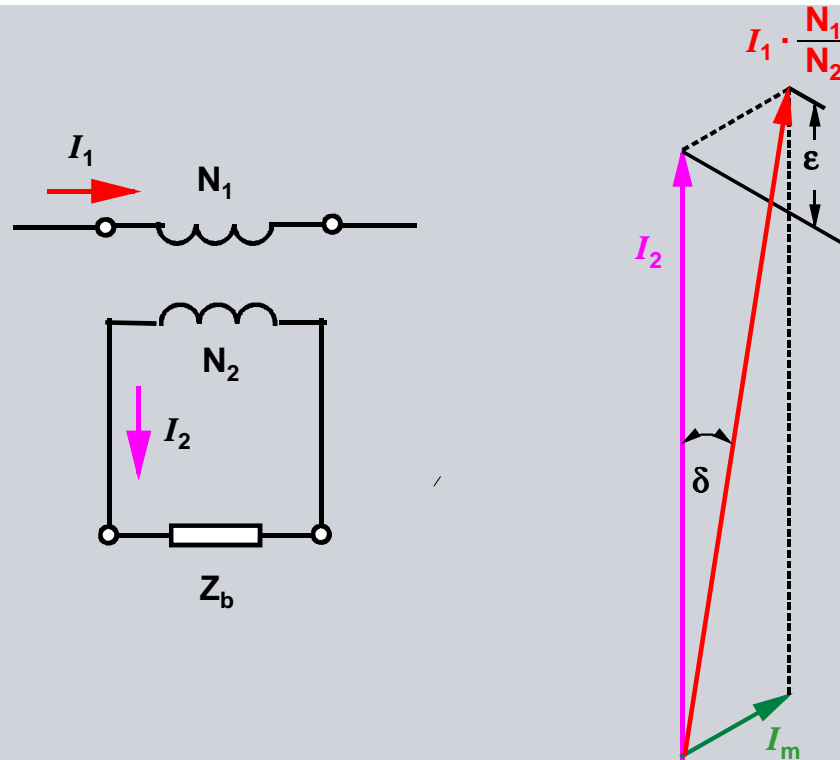
# Current transformer, simplified equivalent circuit



$$I_1' = \frac{1}{N_2} \cdot I_1$$

# Current transformer: Phase displacement ( $\delta$ ) and current ratio error ( $\epsilon$ )

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## Current transformer, Standard for steady-state performance



IEC 60044-1 specifies the following classes:

Accuracy class	Current error at nominal current ( $I_n$ )	Angle error $\delta$ at rated current $I_n$	Total error at $n \times I_n$ (rated accuracy limit)
5P	$\pm 1 \%$	$\pm 60$ minutes	5 %
10P	$\pm 3\%$	—	10 %

## Current transformers, Standard for transient performance

IEC 60044-6 specifies four classes (1992/3):

Class	Error at rated current		Maximum error at rated accuracy limit	Remanence
	Ratio error	Angle error		
TPX (closed iron core)	$\pm 0,5 \%$	$\pm 30 \text{ min}$	$\hat{\epsilon} \leq 10\%$	no limit
TPY with anti-remanence air gap	$\pm 1,0 \%$	$\pm 60 \text{ min}$	$\hat{\epsilon} \leq 10\%$	< 10 %
TPZ linear core	$\pm 1,0 \%$	$\pm 180 \pm 18 \text{ min}$	$\hat{\epsilon} \leq 10\%$ (a.c. current only)	negligible
TPS closed iron core	Special version for high impedance protection (Knee point voltage, internal secondary resistance)			No limit

# Current transformer, Standard for steady-state performance



IEC 60044-1 (Edition 1.2 2003) specifies the following classes for low remanence:

Accuracy class	Current error at nominal current ( $I_n$ )	Angle error $\delta$ at rated current $I_n$	Total error at $n \times I_n$ (rated accuracy limit)
5PR	$\pm 1 \%$	$\pm 60$ minutes	5 %
10PR	$\pm 3\%$	—	10 %

The remanence factor  $K_r$  shall not exceed 10%

$$K_r = 100 \cdot \frac{\psi_r}{\psi_s}$$

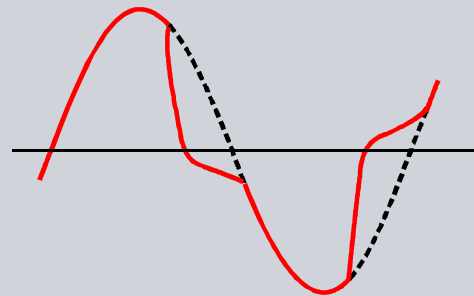
## Current transformer, Class PX

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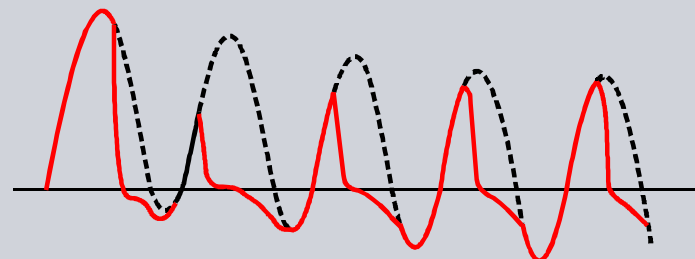
IEC 60044-1 (Edition 1.2 2003) specifies the Class PX:

- Rated turns ratio: turns ratio error  $< 0.25\%$
- Rated knee point emf.
- Max exciting current at rated knee point emf. And/or at a stated percentage thereof
- Max resistance of secondary winding

# Current transformer saturation

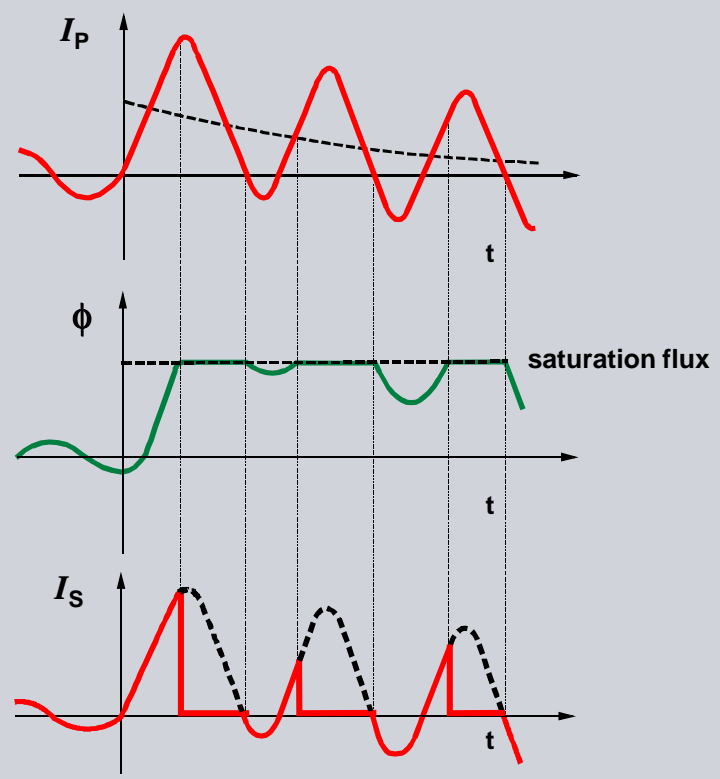


Steady-state saturation with AC current

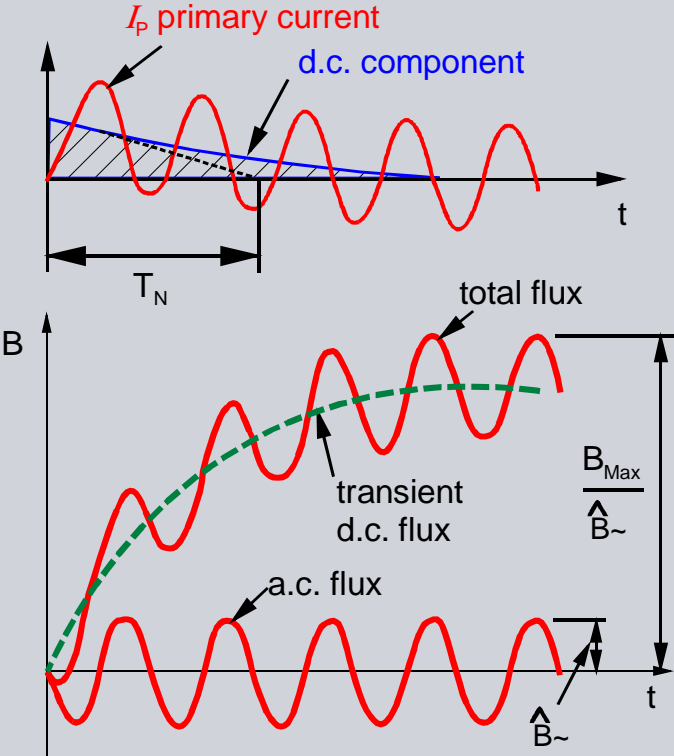


Transient saturation with offset current

# CT saturation Currents and magnetising



Course of CT-flux during off-set short-circuit current



$$\frac{B}{\hat{B}_{\sim}} = 1 + \frac{\omega \cdot T_N \cdot T_S}{T_N - T_S} \left( e^{-\frac{t}{T_N}} - e^{-\frac{t}{T_S}} \right)$$

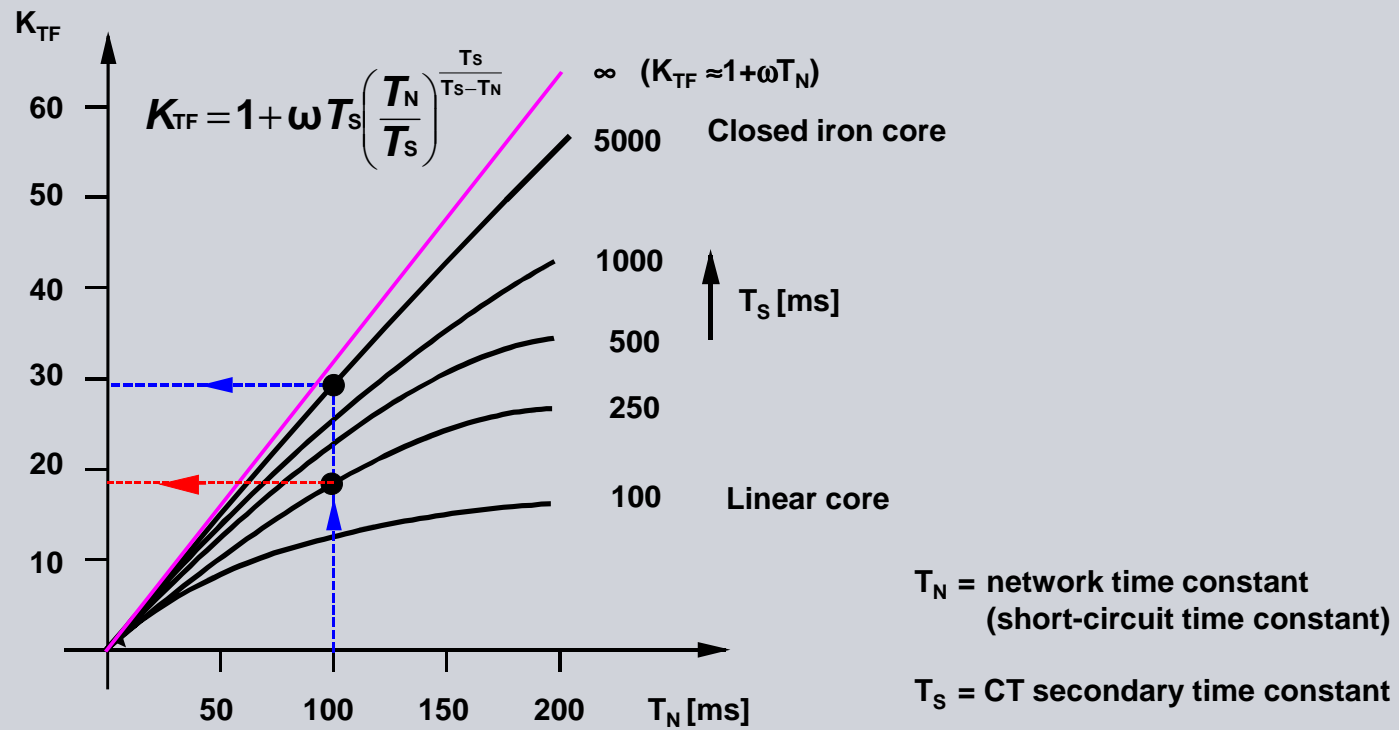
$$\frac{B_{Max}}{B_{\sim}} = 1 + \omega \cdot T_S \cdot \left( \frac{T_N}{T_S} \right)^{\frac{T_S}{T_S - T_N}}$$

$$t_{B_{Max}} = \frac{T_N \cdot T_S}{T_S - T_N} \cdot \ln \frac{T_S}{T_N}$$

$$T_S = \frac{L_w}{R_i + R_B} = \frac{1}{\omega \cdot \tan \delta}$$

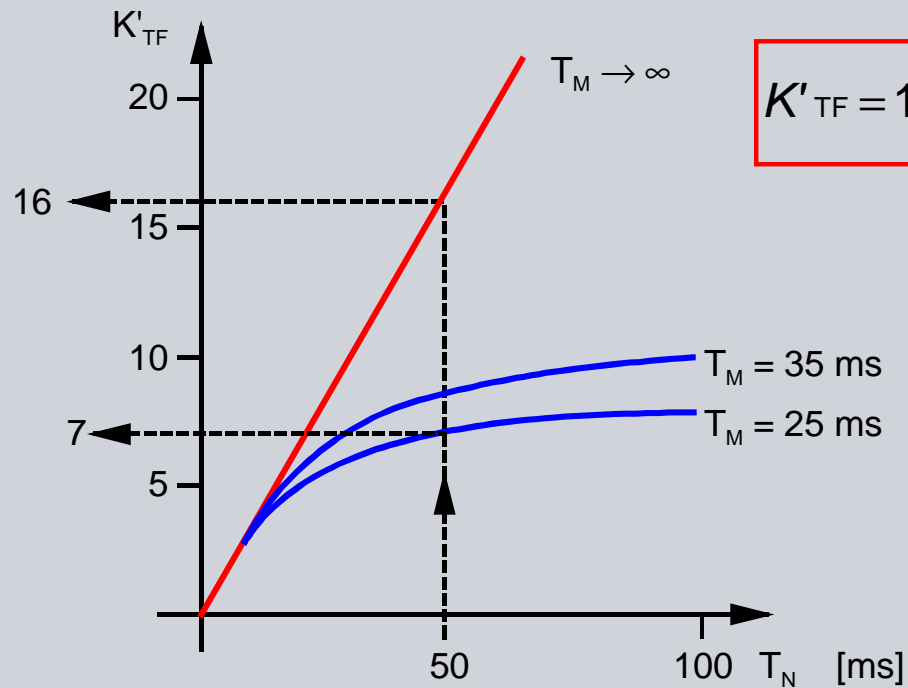
For 50 Hz:  $T_S = \frac{10900}{\delta_{[min]}} [ms]$

CT transient over-dimensioning factor  $K_{TF}$



CT with closed iron core,  
Over-dimensioning factor for a specified time to saturation ( $T_M$ )

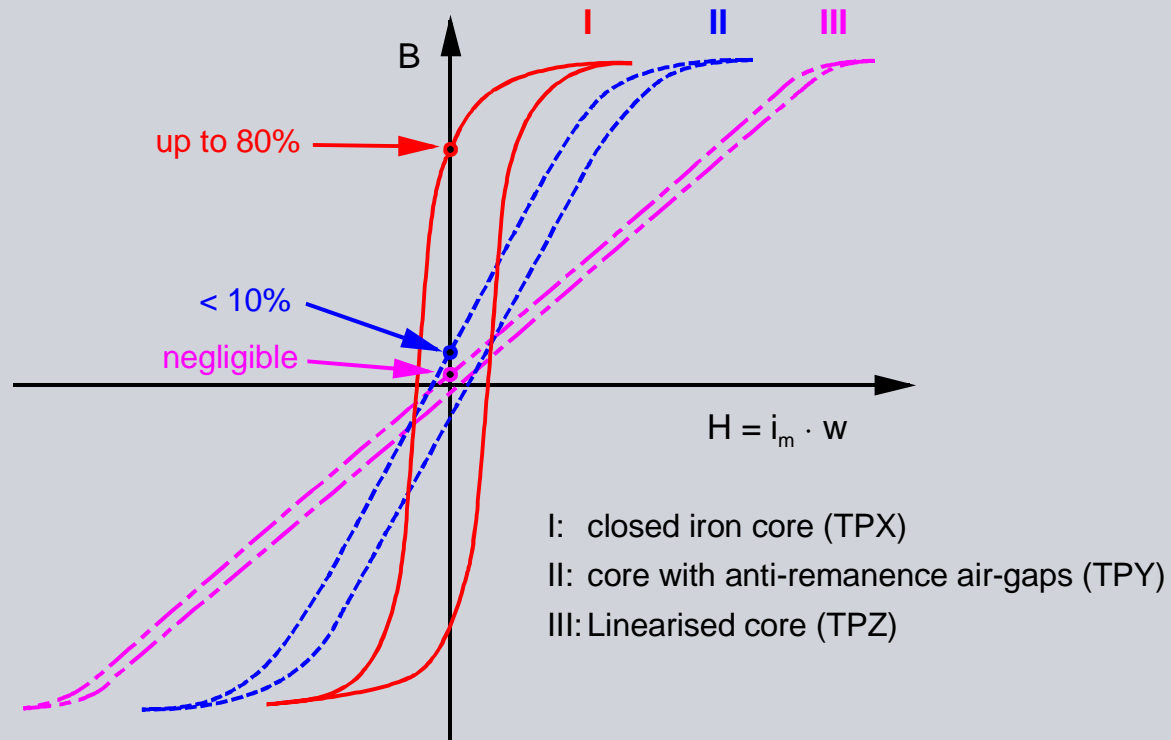
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$$K'_{TF} = 1 + \omega T_N = 1 + \frac{X_N}{R_N}$$

$$K'_{TF} = 1 + \omega T_N \left( 1 - e^{-\frac{T_M}{T_N}} \right)$$

# Current transformer magnetising curve and point of remanence



# Standards of voltage transformers



VT classes to IEC 60044-3

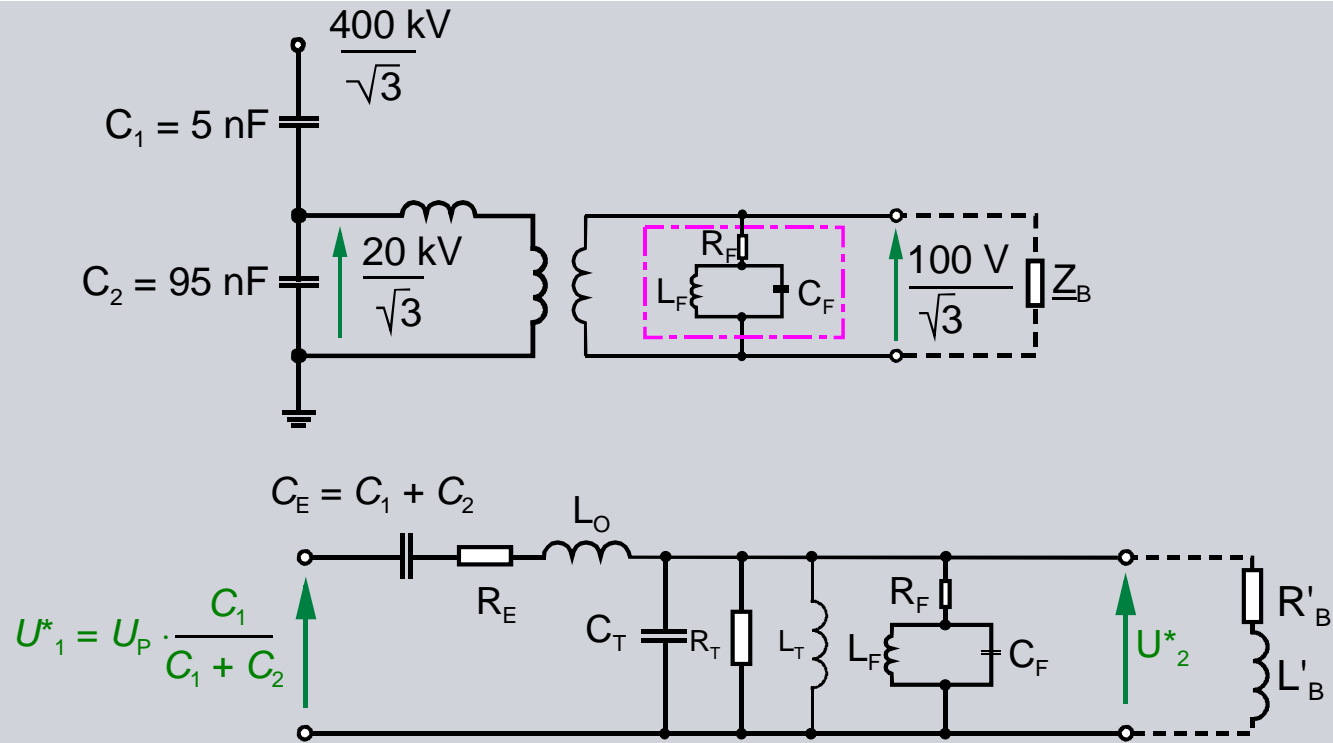
Class designation	Permissible error at $0.05 \cdot U_N$ and $1.0 \cdot U_N$	
	Voltage error $F_U$	Angle error $\delta$
3P	$\pm 3.0 \%$	120 minutes
5P	$\pm 6.0 \%$	240 minutes

VT classes for measurement and protection VDE 0141, Teil 3

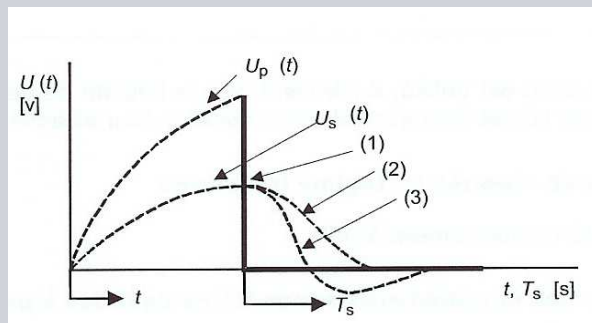
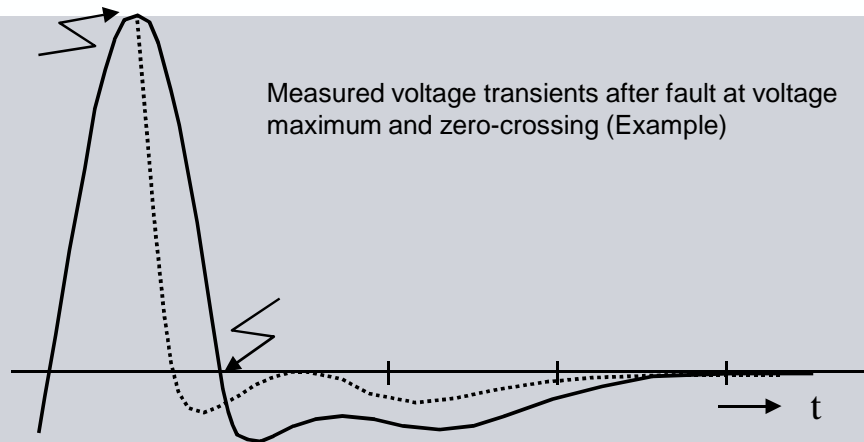
Class designation	Permissible voltage error in %		Permissible angle error in minutes	
	at $1.0 \cdot U_N$	at $0.05 \cdot U_N$	at $1.0 \cdot U_N$	at $0.05 \cdot U_N$
0.1	0.1	1.0	5	40
0.2	0.2	1.0	10	40
0.5	0.5	1.0	20	40
1	1	2.0	30	80
3	3	6.0	40	120

# Capacitive voltage transformer, Equivalent circuit

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# Transient performance of CVTs, Recommendations acc. to IEC 60044-5



Legend:

- $U_p(t)$  Primary voltage
- $U_s(t)$  Secondary voltage
- (1) Fault inception
- (2) Aperiodic damping of  $U_s(t)$
- (3) Periodic damping of  $U_s(t)$

Time $T_s$ in ms	Ratio $\frac{U_s(t)}{\sqrt{2} \cdot U_s} \cdot 100\%$		
	Classes		
	3PT1 6PT1	3PT2 6PT2	3PT3 6PT3
10	---	$\leq 25$	$\leq 4$
20	$\leq 10$	$\leq 10$	$\leq 2$
40	$\leq 10$	$\leq 2$	$\leq 2$
60	$\leq 10$	$\leq 0.6$	$\leq 2$
90	$\leq 10$	$\leq 0.2$	$\leq 2$

Recommendations to IEC 60044-5

# CT dimensioning

$$ALF' = ALF \cdot \frac{P_i + P_{BN}}{P_i + P_B} = ALF \cdot \frac{R_{CT} + R_{BN}}{R_{CT} + R_B}$$

$$ALF = ALF' \cdot \frac{P_i + P_B}{P_i + P_{BN}} = ALF' \cdot \frac{R_{CT} + R_B}{R_{CT} + R_{BN}}$$

with  $ALF' \geq K_{OD} \cdot \frac{I_K}{I_N}$

$$K_{OD} \geq K_{TF} \cdot K_{Rem}$$

$$K_{Rem} = \frac{1}{1 - \frac{\% \text{ Remanence}}{100}}$$

rated CT burden:  $P_{BN}$   
 internal burden of the CT:  $P_i = R_i \cdot I_{2N}^2$

Actual connected burden :  $P_B = R_B \cdot I_{2N}^2$

$R_B = R_i + R_R =$  burden resistance  
 $R_i =$  resistance of connecting cables  
 $R_R =$  burden resistance of the relay

Theory:

No saturation for the total short-circuit duration:

$$K'_{TF} = \frac{B_{Max}}{\hat{B}} = 1 + \omega T_N = 1 + \frac{X_N}{R_N}$$

No saturation for the specified time  $t_M$ :

$$K''_{TF} = \left[ 1 + \frac{\omega \cdot T_N \cdot T_S}{T_N - T_S} \left( e^{\frac{t_M}{T_N}} - e^{\frac{t_M}{T_S}} \right) \right]$$

Note: this equation is not fully valid for very small  $t_M$  (less than 1 cycle)

Practice: Use of  $K_{TF}$  - values recommended by vendors

## Distance relays, practical CT requirements

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### Transient over-dimensioning factors $K_{TF}$ (ARC not considered)

7SA510 / 511	$\left\{ \begin{array}{l} \text{Close-in fault} \\ \text{Fault at balance point} \end{array} \right.$	$\left\{ \begin{array}{l} K_{TF} \geq 2 \quad \text{if } T_N < 50ms \\ K_{TF} \geq 3 \quad \text{if } 50ms \leq T_N < 100ms \\ K_{TF} \geq 10 \end{array} \right.$
7SA513	$\left\{ \begin{array}{l} \text{Close-in fault} \\ \text{Fault at balance point} \end{array} \right.$	$\left\{ \begin{array}{l} K_{TF} \geq 2 \\ K_{TF} \geq 5 \quad \text{if } T_N < 50ms \\ K_{TF} \geq 10 \quad \text{if } T_N \geq 50ms \end{array} \right.$
7SA6 / 7SA522	$\left\{ \begin{array}{l} \text{Close-in fault} \\ \text{Fault at balance point} \end{array} \right.$	$\left\{ \begin{array}{l} K_{TF} \geq 2 \quad (\geq 1 \text{ if } T_N < 30ms) \\ K_{TF} \geq 5 \end{array} \right.$

# 7SA6 / 7SA522: Operating time with CT saturation Influence of CT dimensioning

